

Mai 2008.

I. Cours. ① $\vec{\text{rot}} \vec{E} + \frac{\partial \vec{B}}{\partial t} = \vec{0}$; $\text{div} \vec{B} = 0$; $\text{div} \vec{E} = \frac{\rho}{\epsilon_0}$; $\vec{\text{rot}} \vec{B} = \mu_0 (\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t})$ (1,5pt)

② $\vec{n}_{12} \wedge (\vec{E}_2 - \vec{E}_1) = \vec{0}$; $\vec{n}_{12} \cdot (\vec{B}_2 - \vec{B}_1) = 0$; $\vec{n}_{12} \cdot (\vec{E}_2 - \vec{E}_1) = \frac{\sigma}{\epsilon_0}$; $\vec{n}_{12} \wedge (\vec{B}_2 - \vec{B}_1) = \mu_0 \vec{J}_s$ (1,5pt)

II. 1) $\phi = B_1 \cdot N_2 (\pi R_2^2) \cos \theta$ (2pts)

2) $d\mathcal{C} = I_2 d\phi = I_2 \cdot B_1 \cdot N_2 (\pi R_2^2) \sin \theta d\theta$. Mais $d\mathcal{C} = \Gamma \cdot d\theta$ d'où $\Gamma = B_1 N_2 I_2 (\pi R_2^2) \sin \theta$. (2pts)

3) $\vec{M}_2 = I_2 \cdot N_2 (\pi R_2^2) \cdot \vec{n}$. Or $d\mathcal{C} = d(-\vec{M}_2 \cdot \vec{B}_a) = d(-I_2 N_2 \pi R_2^2 B_1 \cos \theta)$ on retrouve Γ . (2pts)

4) $\vec{B}_1 = \mu_0 n_1 \cdot I_0 \cos \omega t \cdot \vec{e}_z$; $\phi = N_2 (\pi R_2^2) \cdot B_1$ est le flux de \vec{B}_1 à travers la spire 2; $e = -\frac{d\phi}{dt}$ (Faraday) $= N_2 (\pi R_2^2) \mu_0 n_1 I_0 \omega \sin \omega t$ (2pts)

III. 1) Continuité de la composante tangentielle de \vec{E} et champ électrique nul dans un conducteur parfait $\Rightarrow \vec{E}_r(z=0) + \vec{E}_i(z=0) = \vec{0}$ d'où $\vec{E}_{r,0} = -E_0 \cdot \vec{e}_x$. (1pt)

2) $\vec{E} = \vec{E}_i + \vec{E}_r = E_0 e^{i(kz - \omega t)} \vec{e}_x - E_0 e^{i(kz - \omega t)} \vec{e}_x = 2i E_0 \sin kz \cdot e^{-i\omega t} \vec{e}_x = 2 E_0 \sin kz e^{i(\frac{\pi}{2} - \omega t)} \vec{e}_x$ (1pt)

et $\vec{E} = 2 E_0 \sin kz \sin \omega t \vec{e}_x$ avec $E_y = E_z = 0$.

3) $\vec{B}_i = \frac{\vec{k} \times \vec{E}_i}{\omega} = \frac{1}{\omega} k \vec{e}_z \times E_0 e^{i(kz - \omega t)} \vec{e}_x = \frac{E_0}{c} e^{i(kz - \omega t)} \vec{e}_y$ (avec $\omega = ck$)

$\vec{B}_r = \frac{\vec{k} \times \vec{E}_r}{\omega} = -\frac{k}{\omega} \vec{e}_z \wedge (-E_0) e^{i(kz - \omega t)} \vec{e}_x = \frac{E_0}{c} e^{i(-kz - \omega t)} \vec{e}_y$ (1pt)

$\vec{B} = \vec{B}_i + \vec{B}_r = 2 \frac{E_0}{c} \cos kz e^{-i\omega t} \vec{e}_y$ et $\vec{B} = \frac{2 E_0}{c} \cos kz \cdot \cos \omega t \cdot \vec{e}_y$ (1pt)

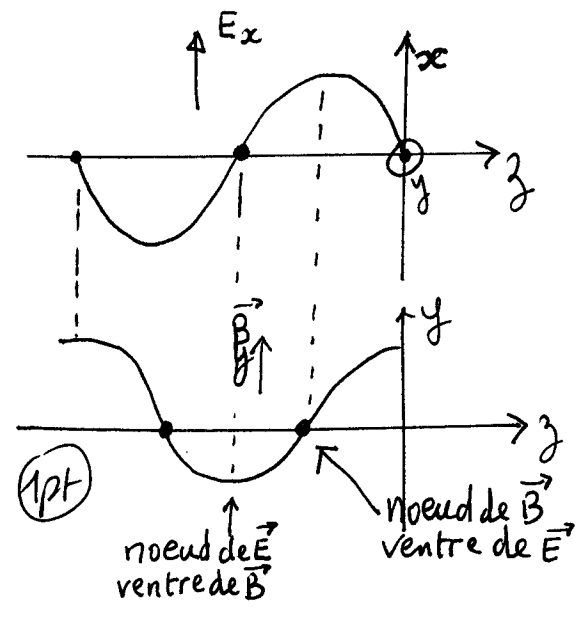
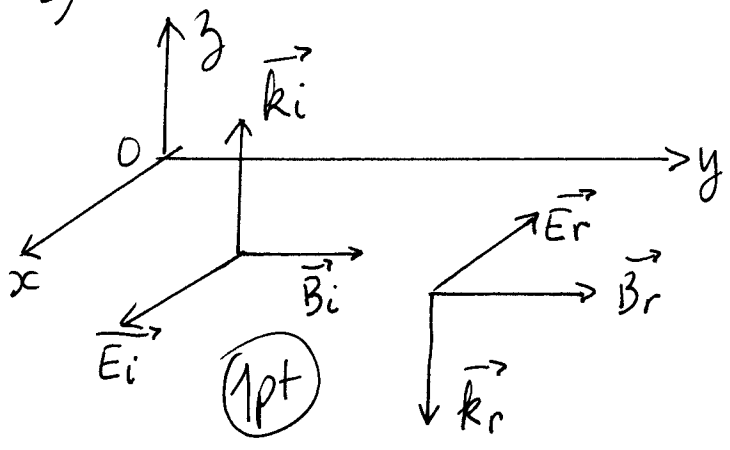
4) $\vec{R} = \frac{1}{\mu_0} \vec{E} \times \vec{B} = \frac{1}{\mu_0} \cdot 2 E_0 \sin kz \cdot \sin \omega t \vec{e}_x \times 2 \frac{E_0}{c} \cos kz \cdot \cos \omega t \vec{e}_y$

$\vec{R} = \frac{4 E_0^2}{\mu_0 c} \sin kz \cdot \cos kz \cdot \sin \omega t \cdot \cos \omega t \cdot \vec{e}_z$ (1pt)

$\langle \vec{R} \rangle_T = \frac{4 E_0^2}{\mu_0 c} \sin kz \cdot \cos kz \langle \sin \omega t \cdot \cos \omega t \rangle_T \vec{e}_z$

$\langle \vec{R} \rangle = 0$ (1pt)

5)



6) On a $\vec{n}_{12} \wedge (\vec{B}_2 - \vec{B}_1) = \mu_0 \vec{J}_s$ soit :

$$\vec{e}_z \times \left[\vec{0} - \frac{2E_0}{c} \cos \omega t \vec{e}_y \right] = \mu_0 \vec{J}_s \quad \text{d'où}$$

dans le conducteur parfait

$$\vec{J}_s = \frac{2E_0}{\mu_0 c} \cos \omega t \vec{e}_x = E_0 \cdot 2 \epsilon_0 c \cdot \cos \omega t \cdot \vec{e}_x$$

(1pt)